

Numerical simulation of turbulent flow over a cavity for fundamental and applied purposes



Alexey Duben, Tatiana Kozubskaya, Natalya Zhdanova

*Keldysh Institute of Applied Mathematics RAS,
Computational AeroAcoustics Laboratory
Moscow, Russia*

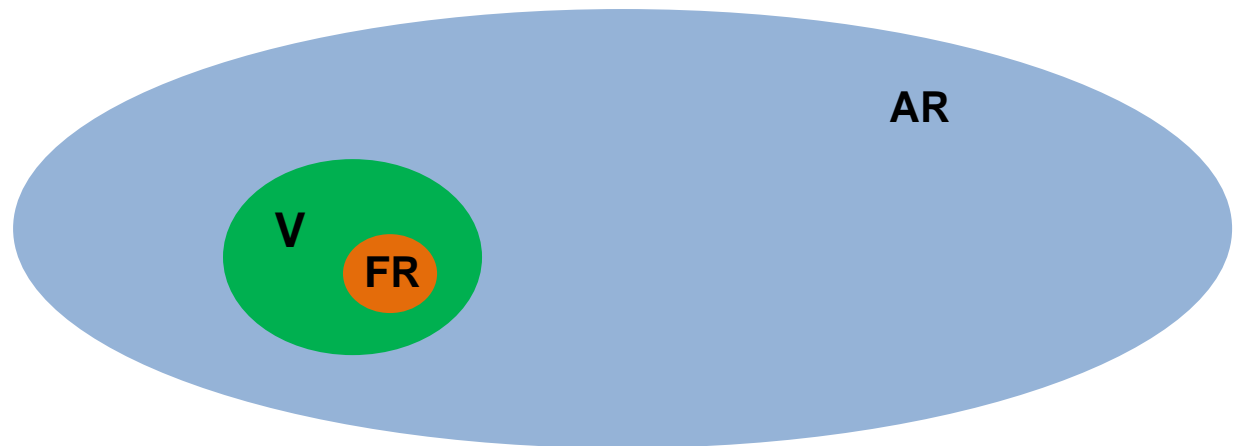


Boris Dankov

TsNIIMash, Korolev, Moscow region, Russia

- **Introduction**
- **Numerical algorithms**
- **Simulation of turbulent flow over cavity M219** as a case for validation
- **Analysis of numerical space-time data** for better understanding of flow physics
- **Prediction of turbulent flow over the cavity with a deflector** as an example of relevant industry-oriented problems
- **Concluding remarks**

- **Computational experiment in aeroacoustics** is the main subject under consideration at the workshop
- **Validation (V) of numerical algorithms and the corresponding codes** is a crucial condition for making computational algorithm:
 - **a means of fundamental research (FR)** and deeper understanding of flow physics;
 - **a means of applied research (AR)** and solving industry-oriented problems



- In the talk we demonstrate this scheme on example of problems connected with **turbulent flows over a cavity**

- **Vertex-centered FV unstructured in-house code NOISEtte**
for solving CFD and CAA problems:
 - turbulent flow simulation using scale-resolving approaches
 - unstructured meshes (tetrahedrons, pyramids, prisms, hexahedrons)
 - O(100K) cores parallel scalability
- **Recent modification [Shur et al., 2015] of hybrid RANS-LES DES method (with $\Delta = \Delta_{SLA}$, shear layer adapted LES length scale)**
which accelerates RANS-to-LES transition in shear layers
- **The algorithm is based on higher-accuracy EBR (Edge-Based Reconstruction) scheme which exploits quasi-1D reconstruction of variables**
- **Remarkable details:**
 - hybrid CD-Upw adaptation of EBR scheme to solution;
 - adaptive change of EBR scheme stencil width depending on the mesh peculiarities (extended or compact stencils in “problem” regions)
- **Time integration: 2nd order implicit scheme (Newton iterations + BiCGStab solver)**
- **Immersed boundary conditions** for installed devices of complicated shapes and/or moving components

Quasi-1D framework for unstructured meshes

Flow parameters:

$$Re_H = 1.37 \cdot 10^6 \quad M_\infty = 0.85$$

$$H = 0.1016 \text{ [m]} \quad P_\infty = 6.21 \cdot 10^4 \text{ [Pa]}$$

Approach:

- IDDES ($\Delta = \Delta_{SLA}$) [Shur et al., 2015]
- Hybrid CD-Upw EBR vertex-centered scheme

Mesh:

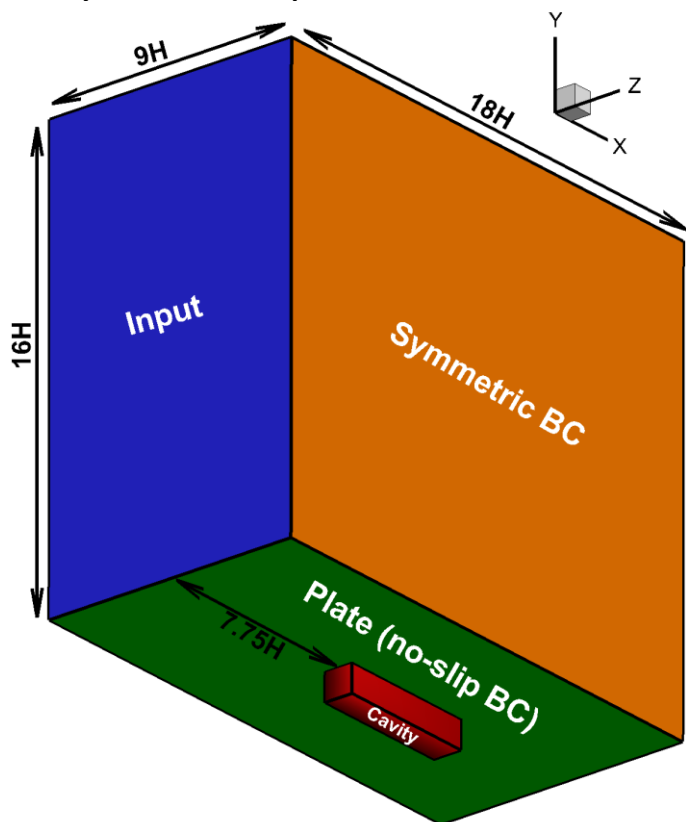
Hexahedral mesh

4M nodes

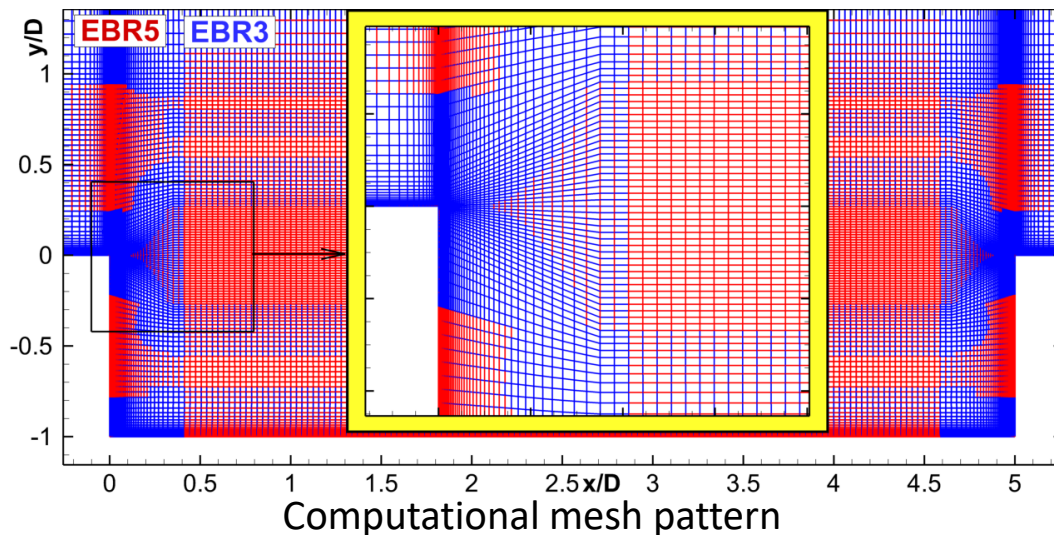
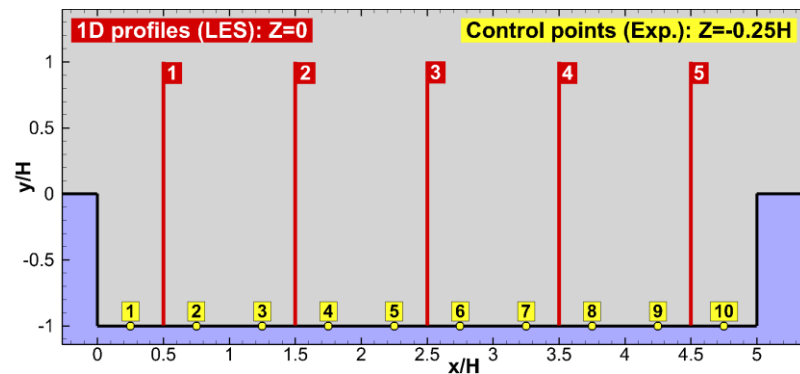
$$\Delta_{LES} = H/33$$

Reference data:

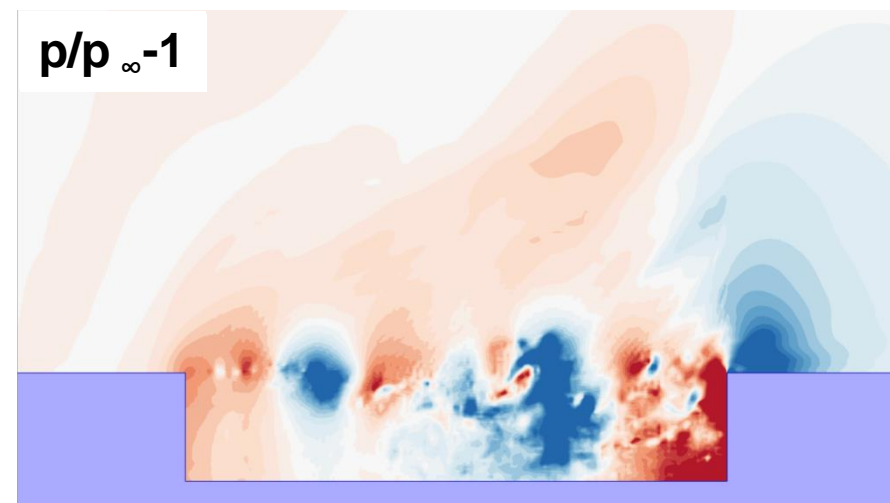
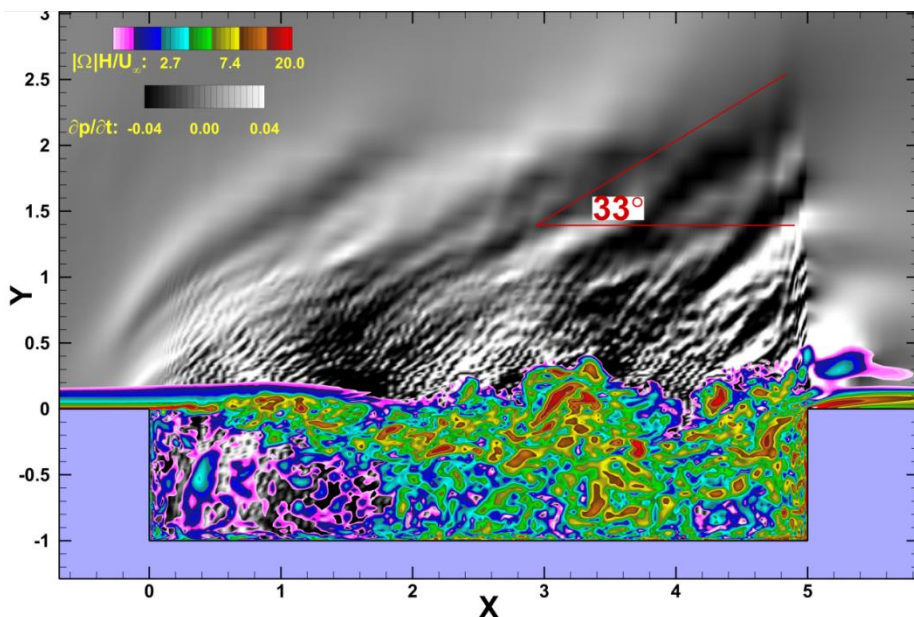
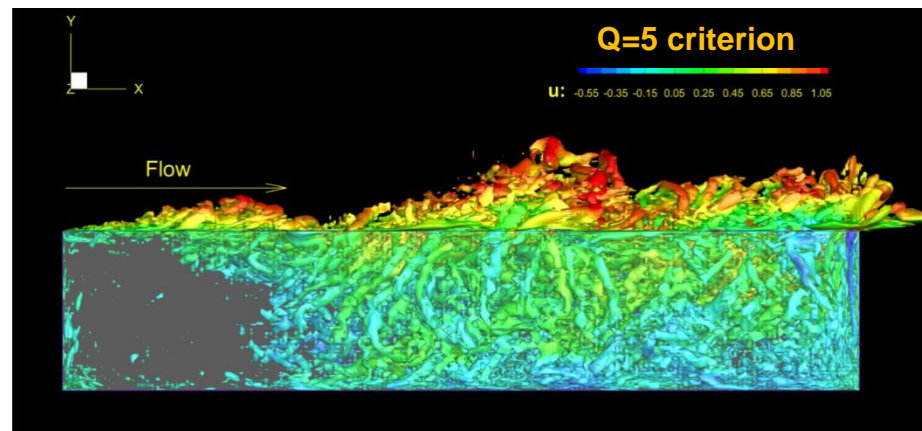
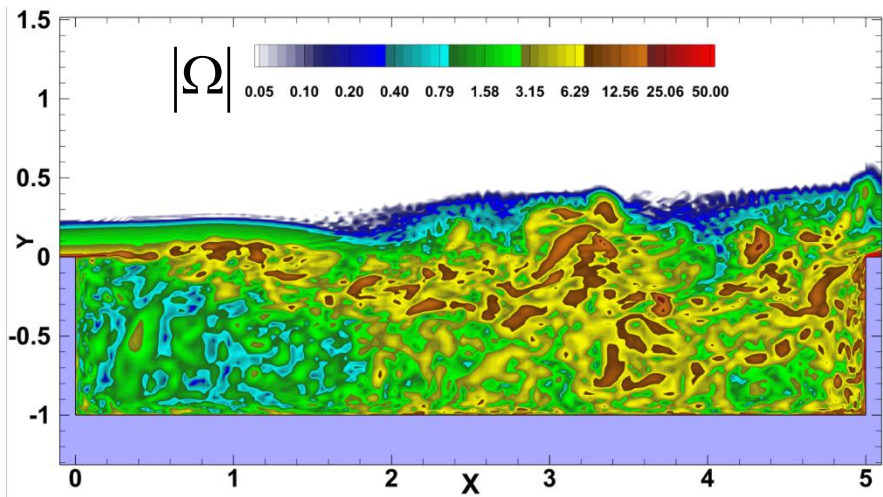
- Experiment: pressure history [de Henshaw et al., 2002]
- LES [Larcheveque et al., 2004]

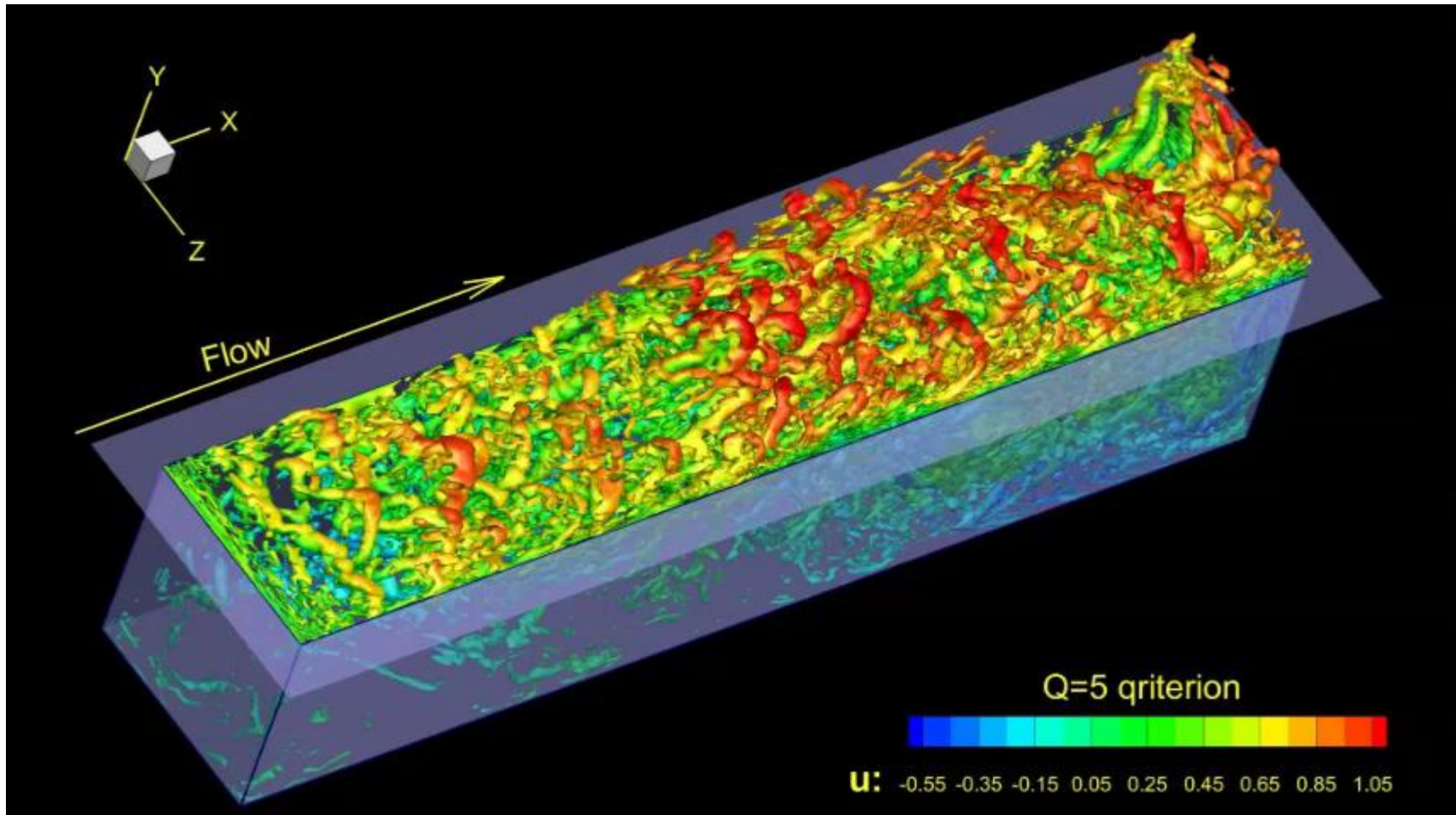


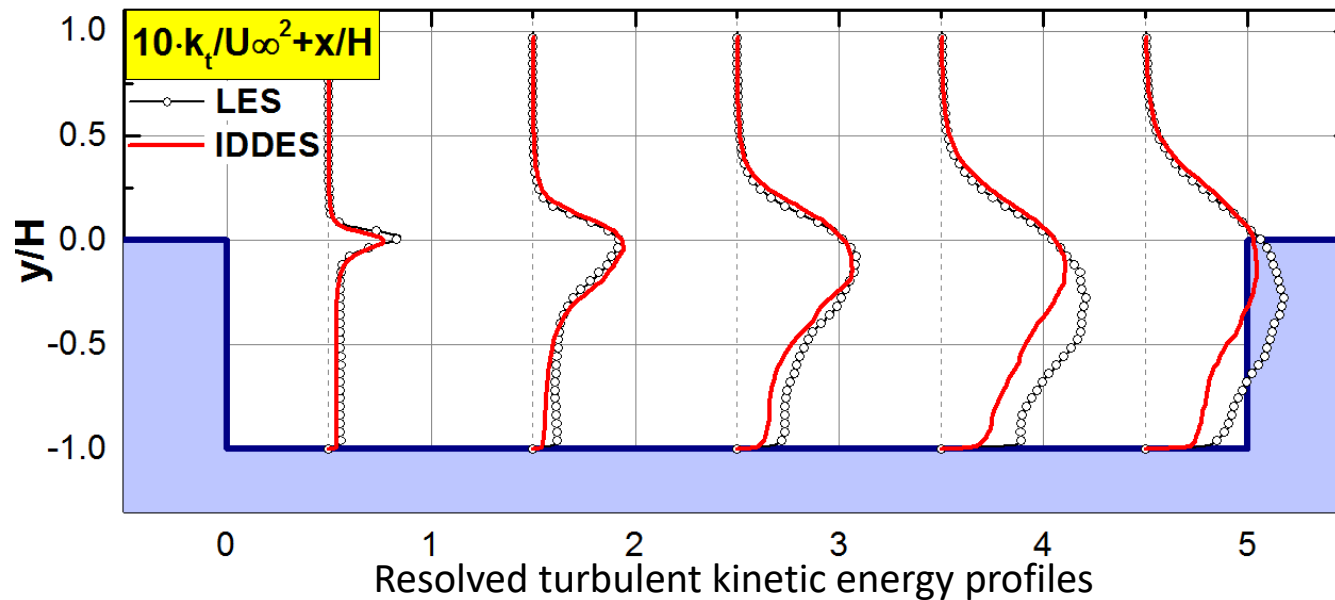
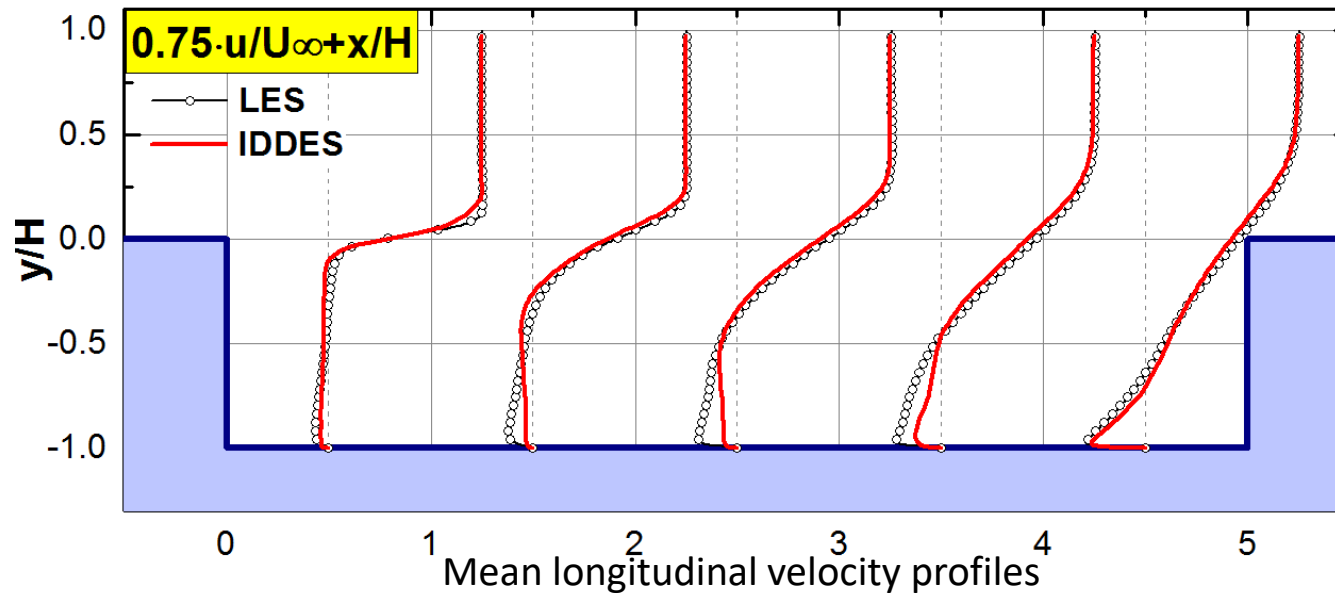
Computational domain



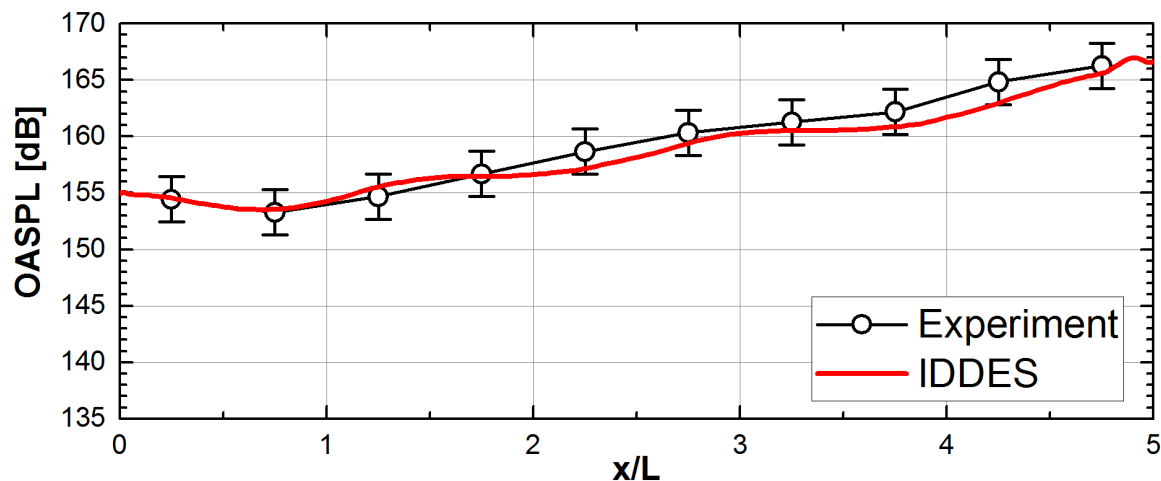
Computational mesh pattern







LES [Larcheveque et al., 2004]

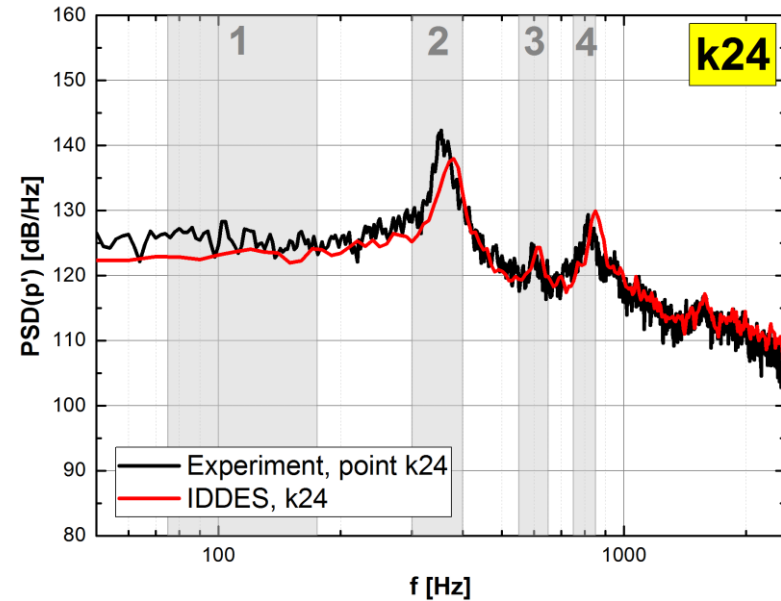
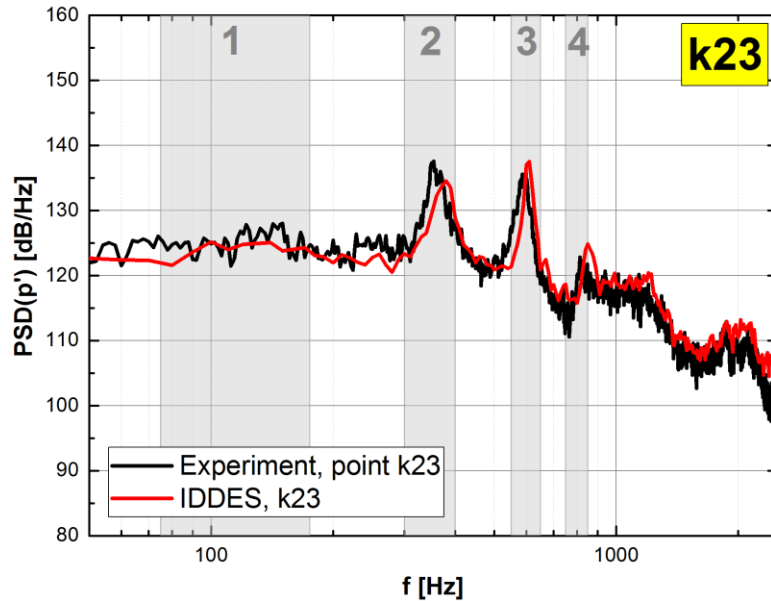
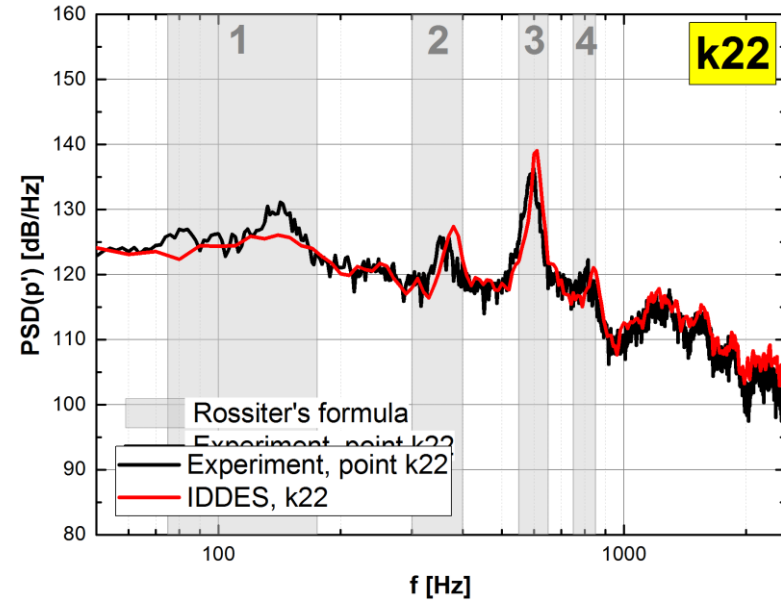
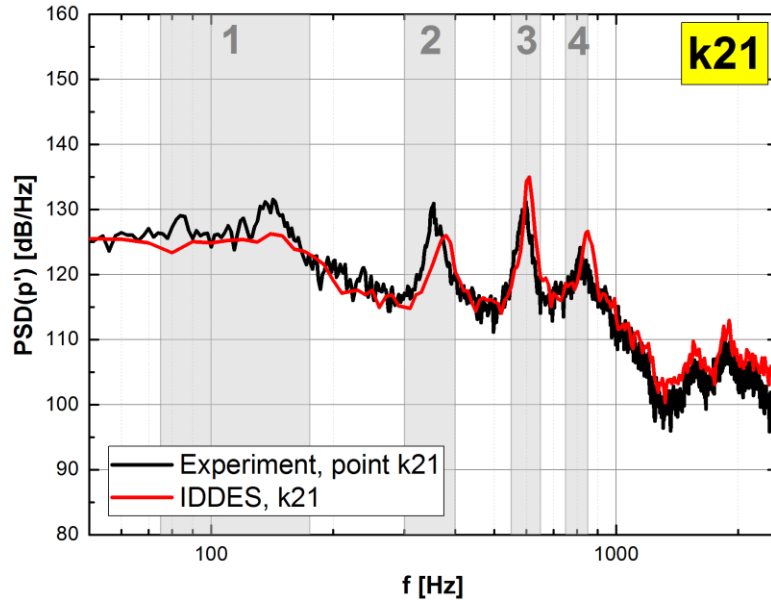


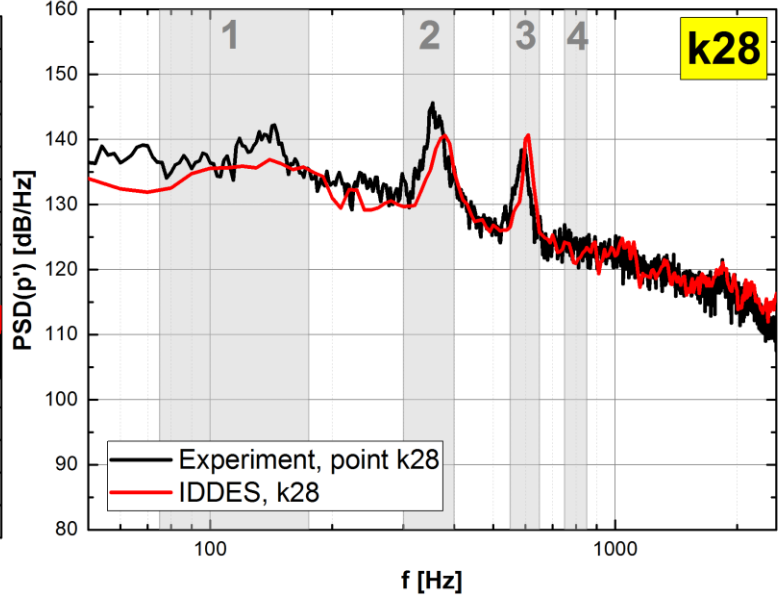
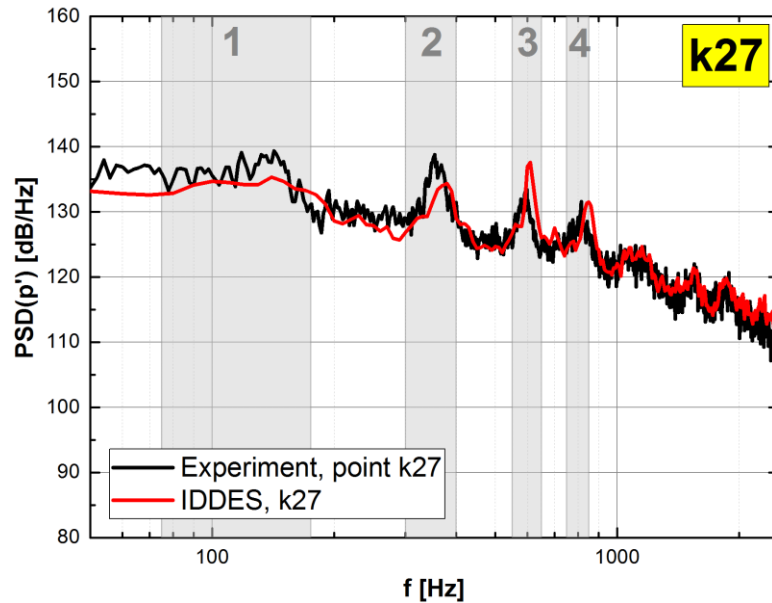
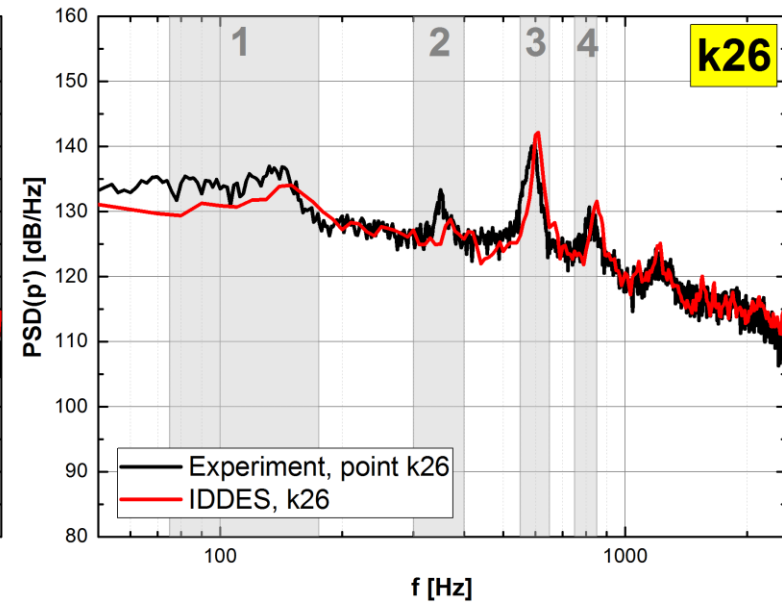
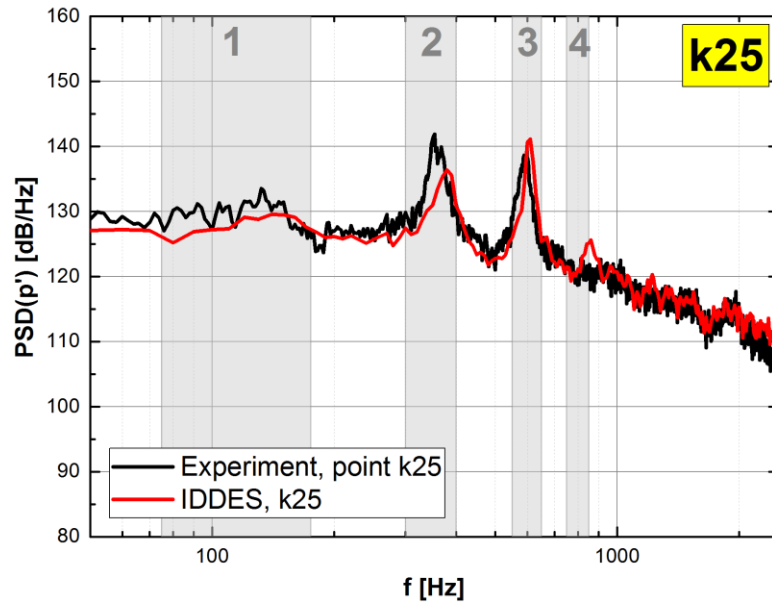
PSD estimation:

- Periodogram method, Hanning window, overlap 50%
- Sample length: experiment: 3.4 [s], IDDES: 1 [s]

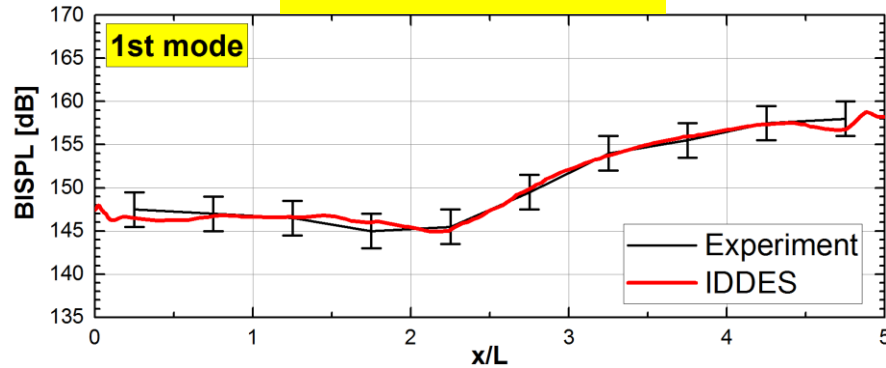
Comparison of Rossiter modes values

Mode	1	2	3	4
Experiment (Hz)	135	350	590	820
Rossiter formula (Hz)	148	357	566	775
LES (Hz)	125	360	585	825
IDDES (Hz)	140	375	595	835

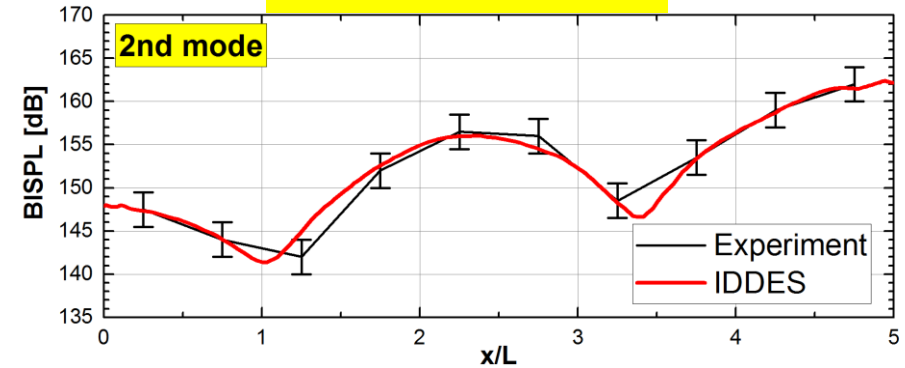




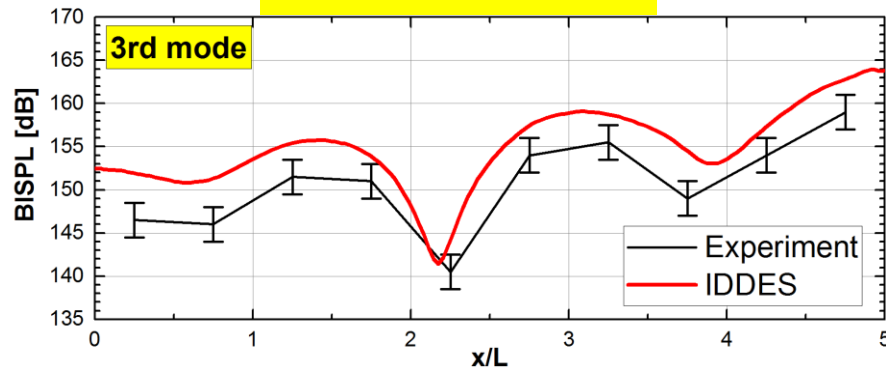
75 Hz f <math>< 175</math> Hz



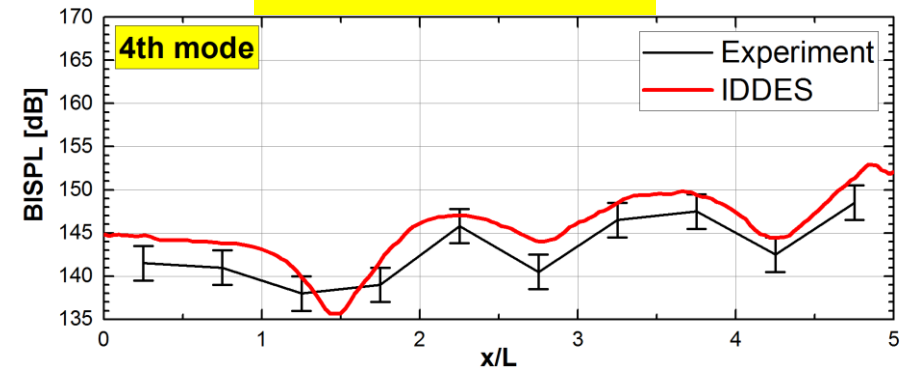
300 Hz f <math>< 400</math> Hz



550 Hz f <math>< 650</math> Hz



750 Hz f <math>< 850</math> Hz



- Results of IDDES are in a good agreement with the experimental data which lets us consider the numerical data **valid**
So, basing on this background, we can do further steps
in the directions of **fundamental** and **applied** research

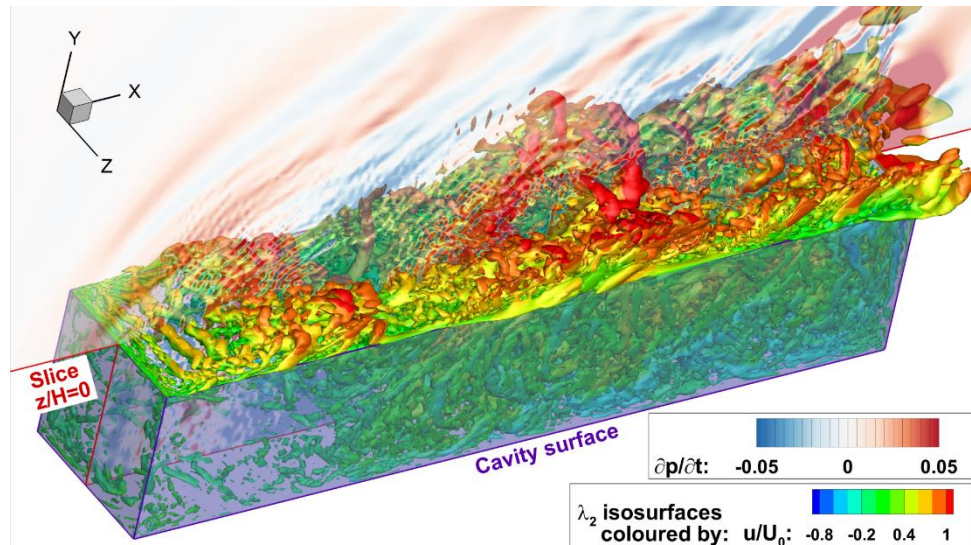
- In [Larcheveque et al., 2004] the detailed analysis of unsteady data accumulated in the process of computation is presented:
 - shear layer mean properties with description of coherent structures dynamics
 - spectral, cross-spectral and bispectral analysis of shear layer
 - pressure spectra analysis on the cavity bottom
 - joint time-frequency analysis to characterize the “mode switching” phenomenon

• In [T. Knacke & F. Thiele, AIAA 2013-2162] the slat noise generation is analyzed

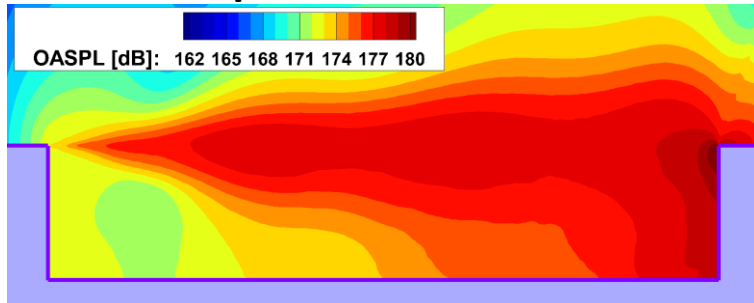
- 1 sec of unsteady data (p' , u' , v' , w' , p') at slice $z/H=0$ and cavity surface has been accumulated during the IDDES computation
- The analysis is mostly based on normalized space-time cross-correlation function

$$R_{pp}(\mathbf{x}_0, \mathbf{x}, \tau) = \frac{\langle p'(\mathbf{x}, t) \cdot p'(\mathbf{x}_0, t + \tau) \rangle}{p'_{\text{rms}}(\mathbf{x}) \cdot p'_{\text{rms}}(\mathbf{x}_0)}$$

- \mathbf{x}_0 – observer position
- \mathbf{x} - varying position
- τ – time delay

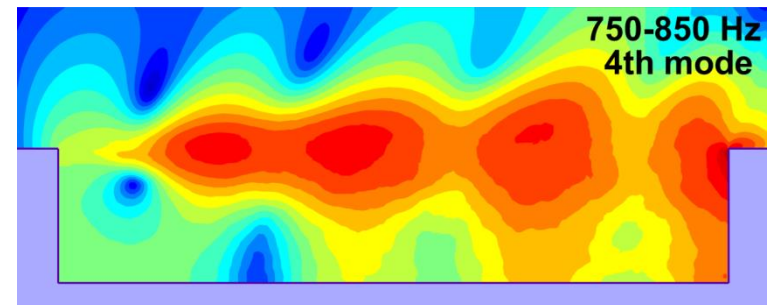
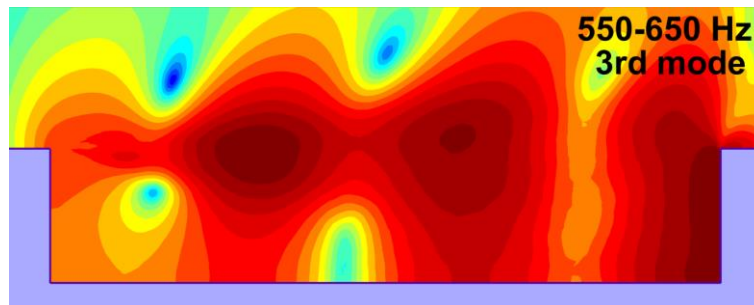
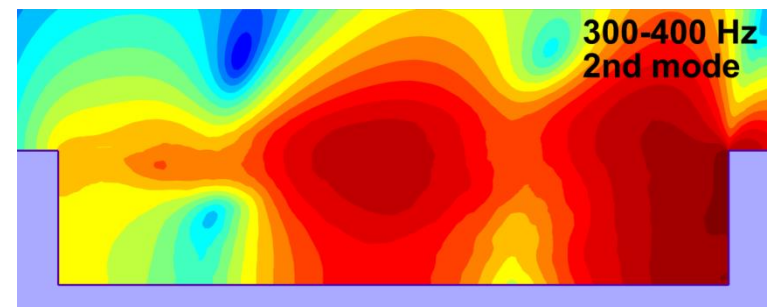
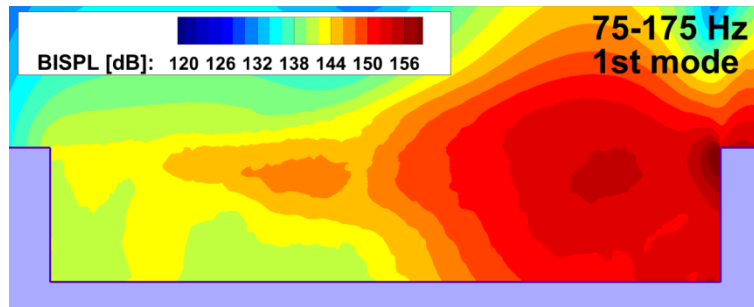


Overall sound pressure level in slice $z/H=0$

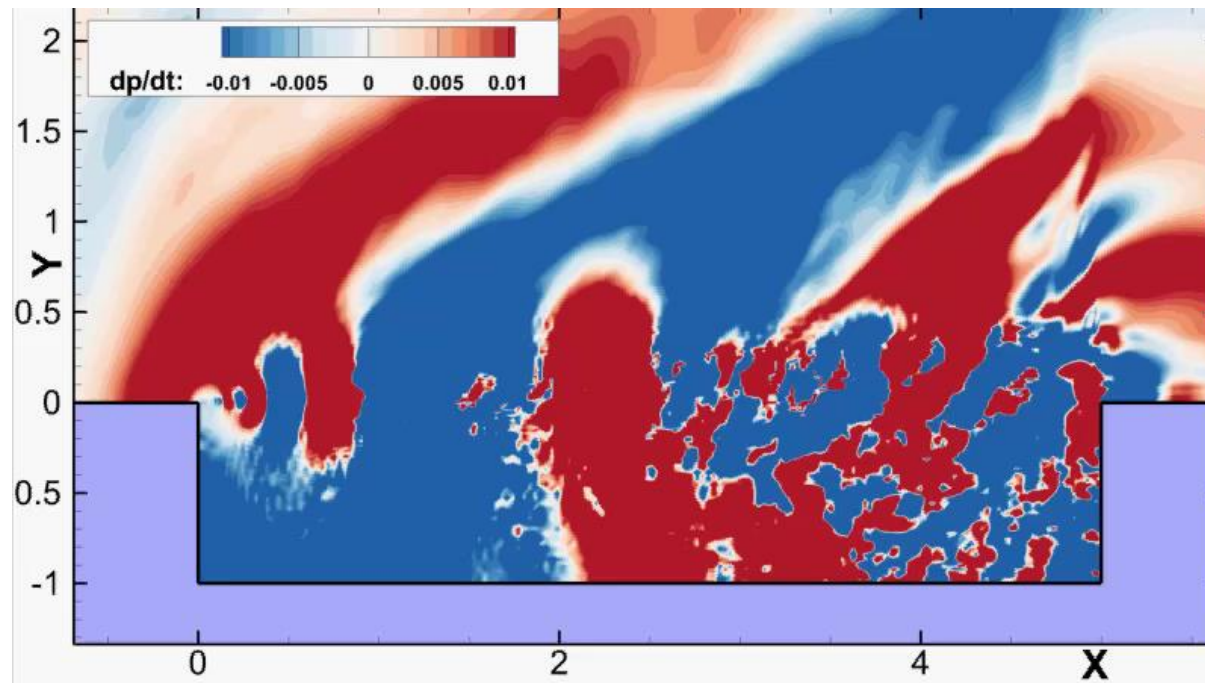


- Includes both turbulent (high frequency) perturbations and acoustic (low frequency) pulsations → identification of acoustics loads is not clear

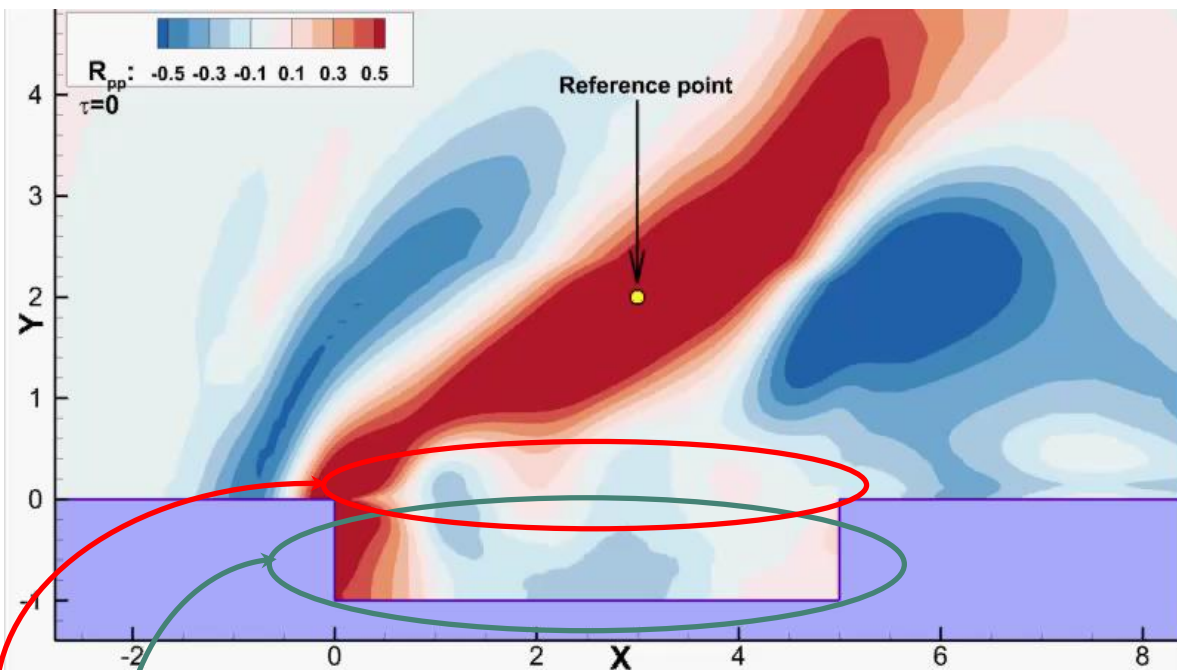
Band-integrated sound pressure level in slice $z/H=0$



- BISPLs show bright spots in the shear layer. They correspond to the Rossiter modes and their quantity depends on the mode numbers
- It looks like standing waves influenced by the shear layer



- Evolution of instantaneous pressure time derivative field is commonly considered as good enough to examine acoustic waves propagation outside main turbulent interaction area. However:
 - in the cavity nearfield acoustic waves (propagating to the farfield) and turbulent disturbances (decaying in the nearfield) are mixed → it's difficult to separate one from another
 - different scales and amplitudes of acoustic and turbulent disturbances also complicate the identification of noise generation mechanisms



$$R_{pp}(\mathbf{x}_0, \mathbf{x}, \tau) = \frac{\langle p'(\mathbf{x}, t) \cdot p'(\mathbf{x}_0, t + \tau) \rangle}{p'_{\text{rms}}(\mathbf{x}) \cdot p'_{\text{rms}}(\mathbf{x}_0)}$$

- High values of R_{pp} (red or blue) correspond to the regions strongly correlated with reference point (\mathbf{x}_0) at time delay τ

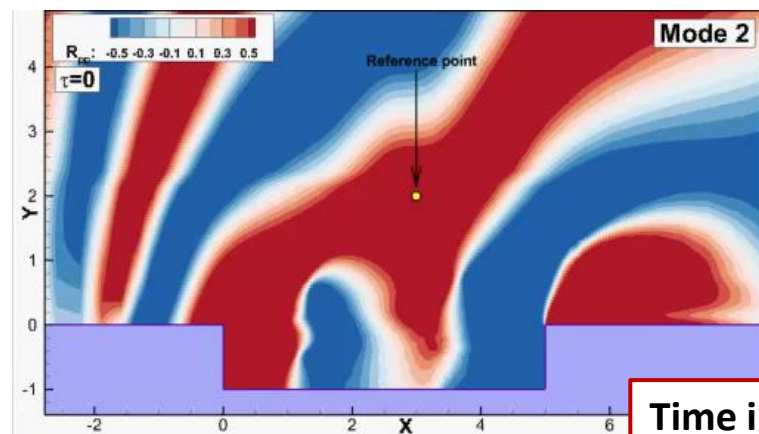
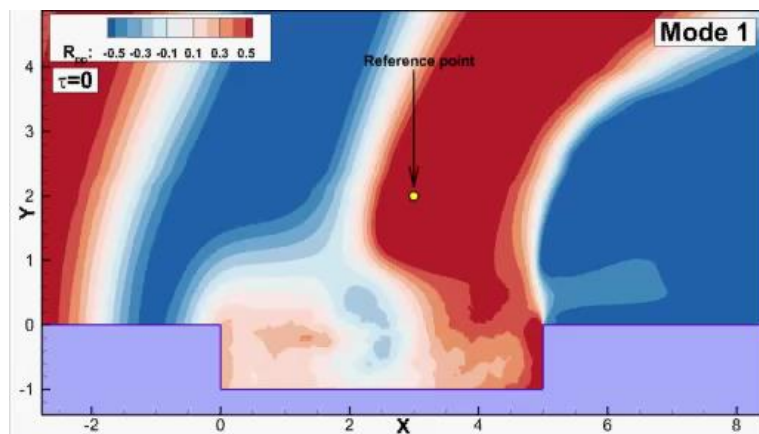
Time in reverse

The main components of self-sustained process of Rossiter modes generation can be seen:

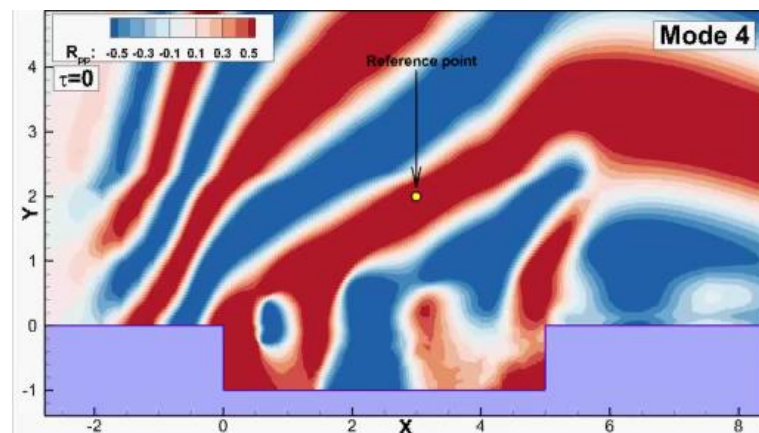
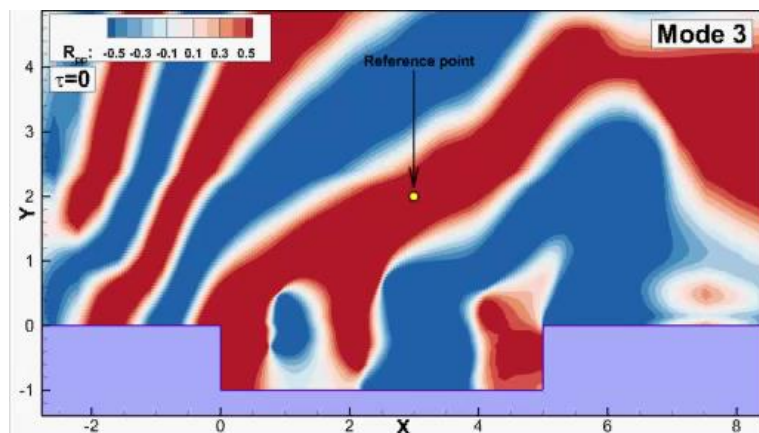
- pressure waves travelling upstream the aft wall which are generated by the interaction of the shear layer with this wall;
- the pressure waves interfere with the leading edge and provoke instability waves in the shear layer

- The movie shows that the outer region and the area inside the cavity are highly correlated, all the flow pattern is involved in the modes generation mechanism
- The decay of correlation in time (the colors become not so bright with time delay) can be explained by floating of Rossiter modes frequencies due to instability of the shear layer

- Band filtered fields provide the information of Rossiter modes generation mechanism much better



Time in reverse



- The movies illustrate well the Rossiter's theory saying that the modulation of the acoustic waves (narrow band noise is amplified) is related with the phase correlation of pressure waves coming upstream from the aft wall and instability waves in shear layers (provoked, in their turn, by upstream pressure waves)

Flow parameters

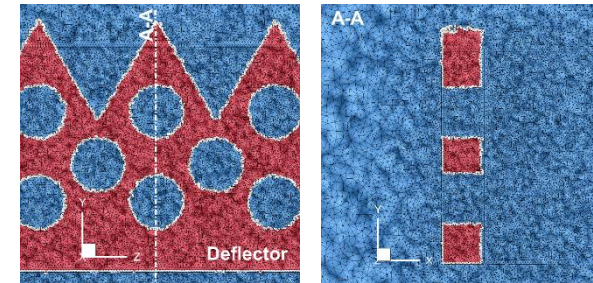
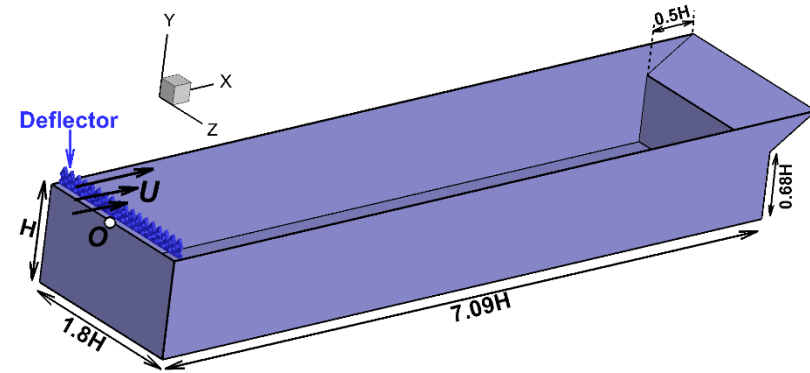
- $Re_H = 7 \cdot 10^6$ (H – cavity depth)
- $M = 0.8$

Approach:

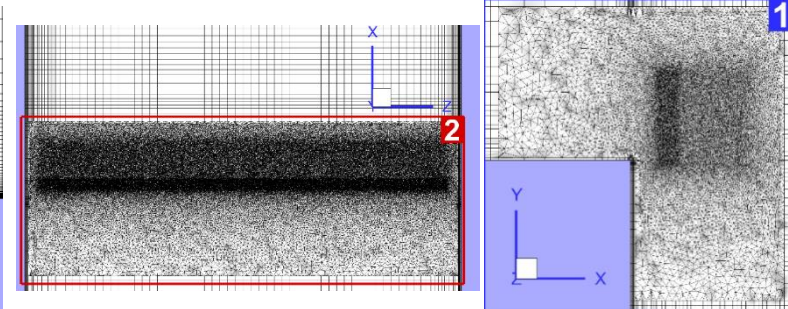
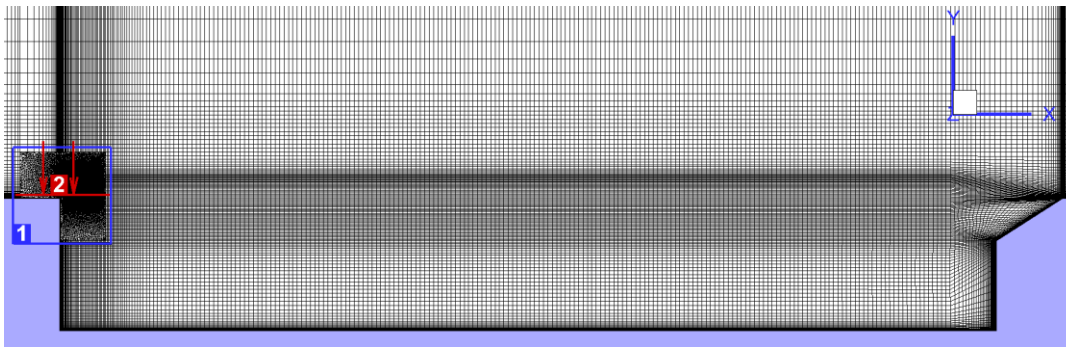
- IDDES ($\Delta = \Delta_{SLA}$) [Shur et al, 2015]
- Hybrid CD-Upw EBR vertex-centered scheme
- Deflector: Immersed Boundary Conditions (IBC) method
- Plate and cavity surfaces: wall functions

Meshes

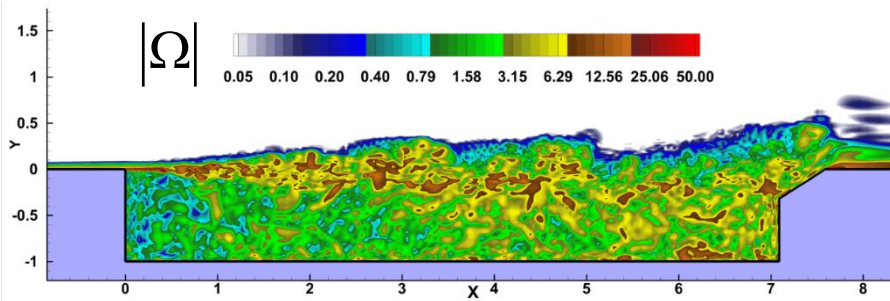
- Cavity without deflector: hexa mesh, 5.07M nodes
- Cavity with deflector: hexa, tetra, pyramids 14.09M nodes
- Cell size:
 - on deflector surface: $8.5 \cdot 10^{-3}h$ ($h=0.215H$)
 - downstream deflector: $\leq h/30$
 - inside cavity: $\leq H/30$



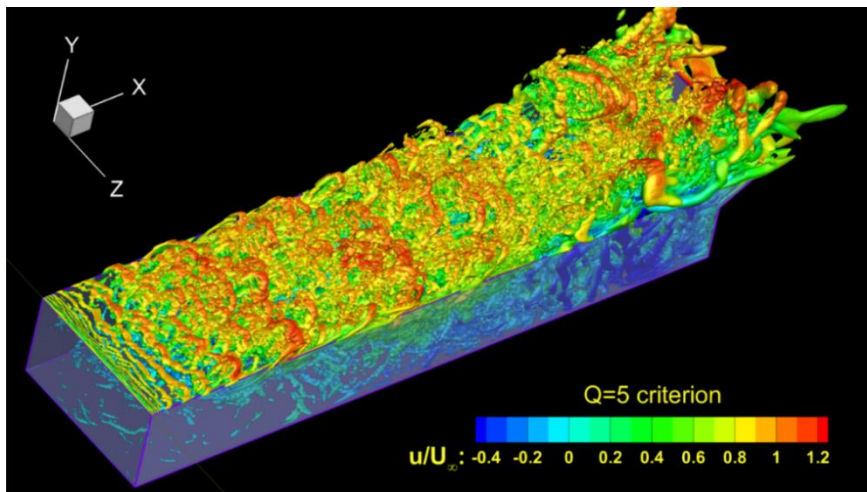
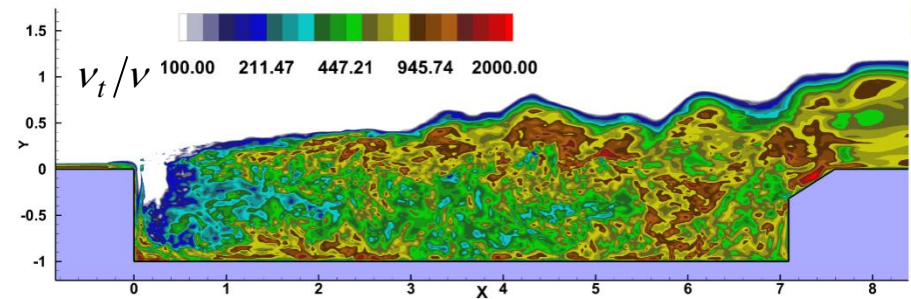
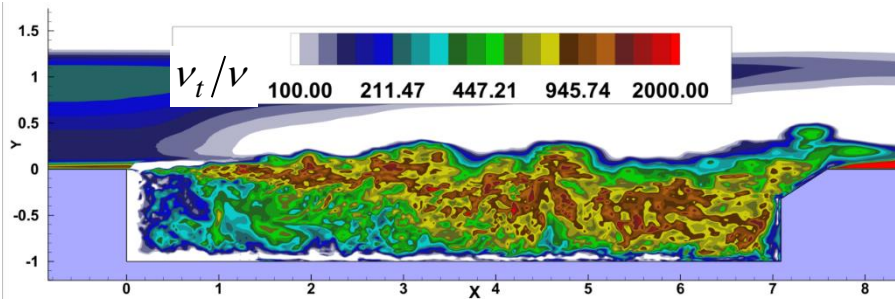
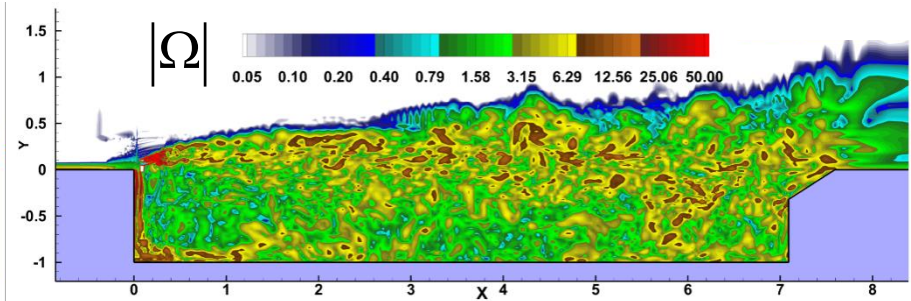
Deflector modelled by IBC (red)



Without deflector

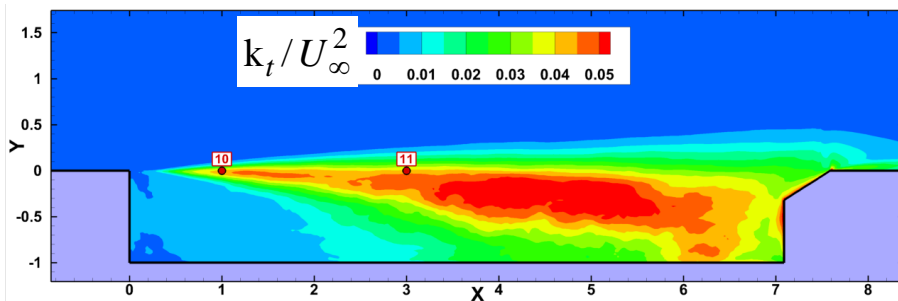
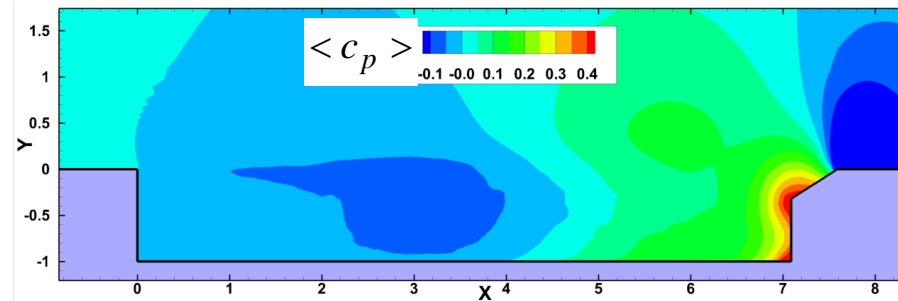
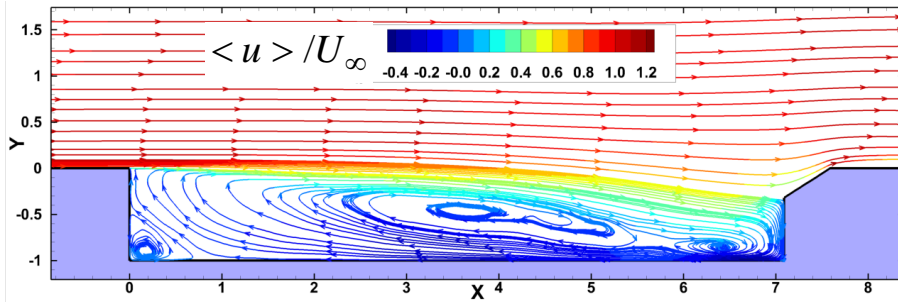


With deflector

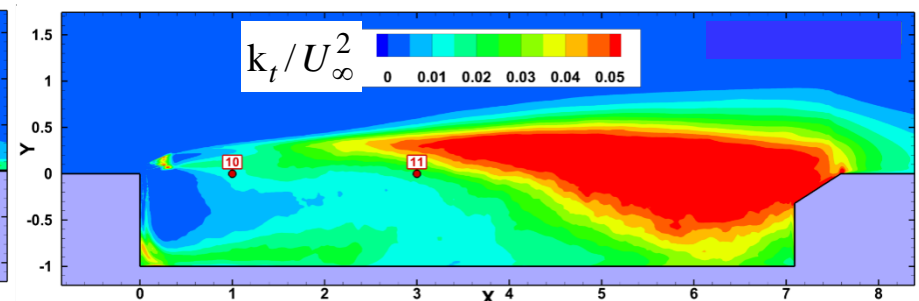
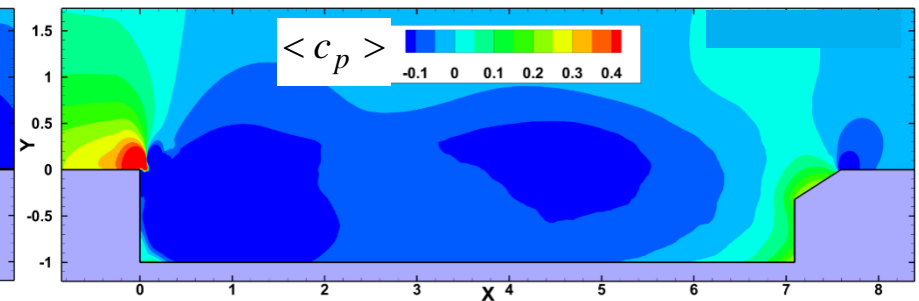
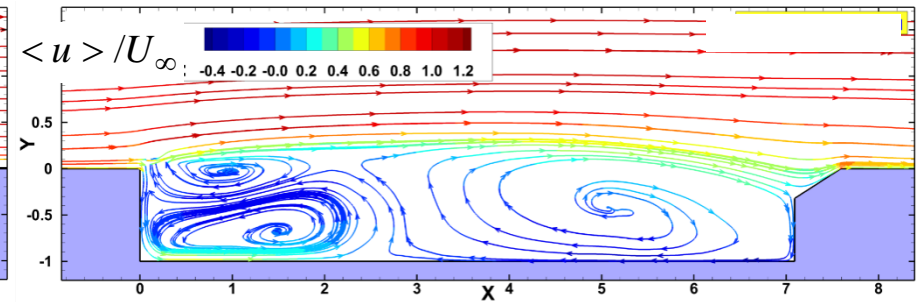


- The RANS-to-LES transition is rather fast in both computations
- The deflector acts as a turbulizer and produces a noticeably thicker developed shear layer

Without deflector



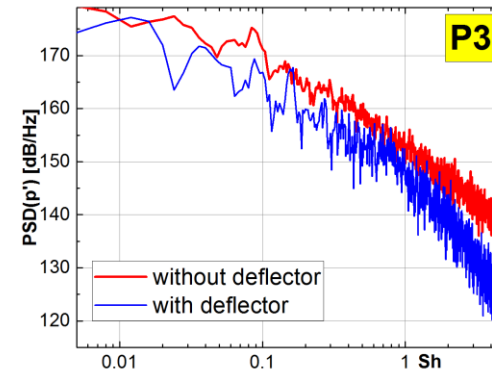
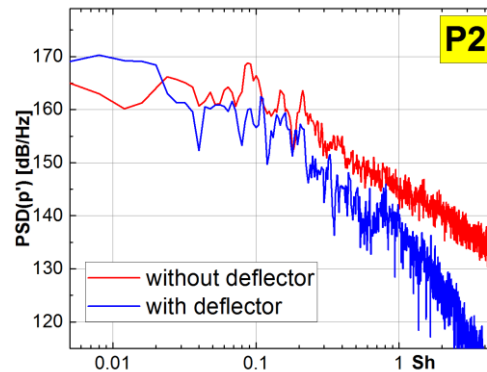
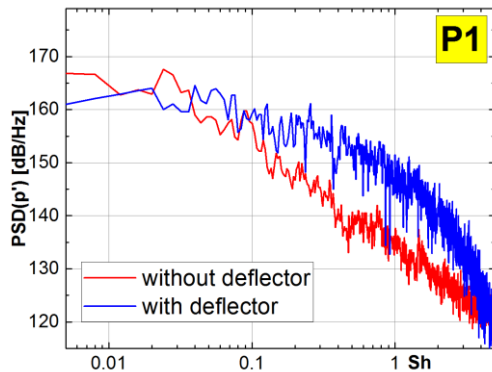
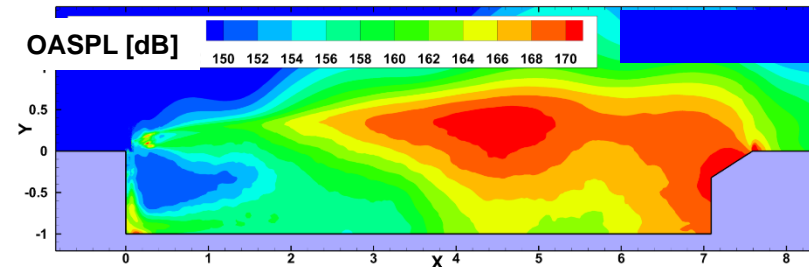
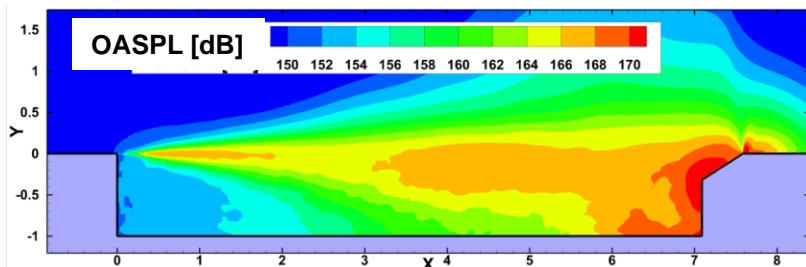
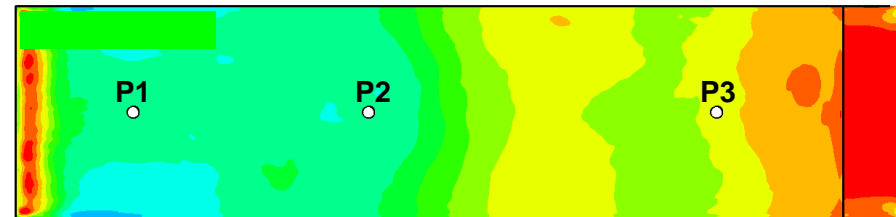
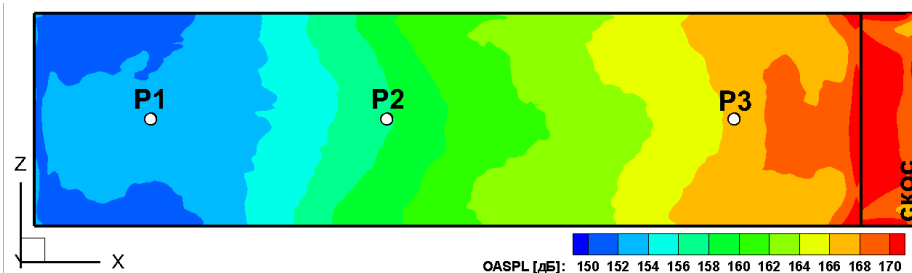
With deflector



- The deflector changes the flow structure: additional recirculation regions appear
- The deflector lowers pressure coefficient on the cavity surface, especially at the aft wall

Without deflector

With deflector



- The deflector changes the distribution of acoustic loads, however not significantly
 - reducing near cavity floor and aft wall edge
 - increasing of SPL near forward vertical wall (flow through the gap between deflector and cavity leading edge)

- We have developed and validated a numerical approach for the prediction of turbulent flow over a cavity using unstructured algorithms
- From fundamental hand side, it opens a possibility for a deeper investigation of cavity flow physics basing on big numerical data analysis. It seems that we are far from the end of this resource and it would be interesting to continue
- From applied hand side, it allow us to carry out predictions for engineering purposes in a certain (even if not so wide) range of problem parameters as long as the next validation step is not needed
- In our case both directions are not completed. So far the presentation can be considered more as a demonstration of ways of computational experiment

Thank you !